preferred, and the coefficient of uniformity could be adjusted by adding a small percentage of finer textured particles, such as native sandy-loam soil. In their studies, increasing the coefficient of uniformity value from 1.8 to 3.0 resulted in a doubling of the sand's bearing capacity – in essence, a much firmer sand root-zone surface. For bunker sands that need to infiltrate and drain rapidly, the addition of significant fines is risky, as it might result in excess water retention and make the sand more prone to erosion when installed on slopes.

In addition to particle size distribution, sand particle shape has a strong influence on playing quality and maintenance. Particle shape is classified by examining the relative sharpness of particle edges and the overall particle shape, referred to as angularity and sphericity (roundness). These characteristics can have a strong influence on surface firmness and resistance to erosion. For example, a low-sphericity, very angular sand generally has a high surface strength and likely will stay in place on bunker faces. By contrast, a high-sphericity, rounded sand is more likely to be soft and prone to erosion during regular maintenance, or following irrigation and rainfall events.

Complicating the bunker sand selection process is that subjective qualitative characteristics, such as color or immediate cost, often strongly influence the final decision with little thought on the possible implications regarding long-term maintenance needs or costs.

The objectives of this laboratory study were to:

1. Characterize the physical properties of a wide variety of commercially available sandsized materials being used in golf course sand bunkers.

2. Determine if certain physical properties can be used as reliable predictors for sand surface hardness or resistance to golf ball penetration as measured using a modified pocket penetrometer.

MATERIALS AND METHODS

Twenty-six sand materials were collected from a variety of sand suppliers throughout the United States (Table 1). About one gallon of each sample was obtained, air-dried and well mixed before analysis. Subsamples (60 grams) from the center of each sand were removed and oven dried to determine particle size distribution using the pipette method and dry sieving on three replicate samples. The remaining sand was used to determine sand firmness, measured by resistance to penetration with a modified pocket penetrometer.

Each sample was placed into the standard measurement vessel (a rigid wooden box with interior dimensions of 11.4 centimeters by 12.7 centimeters) and compacted to a 7.6-centimeter depth. The modified penetrometer was inserted





866-863-3744 • www.underhill.us www.golfcourseindustry.com/readerservice - #53

using even and steady pressure until half the depth of a USGA-approved golf ball was buried. The value was recorded and the device reset. This procedure was replicated five times, and between measurements the sand surface was resmoothed and repacked.

To determine angle of repose, 20-gram samples of oven-dried sand were placed in a 26-millimeter-diameter plastic centrifuge tube with a 5-millimeter-diameter opening at the bottom, mounted perpendicular to a standard microscope stage. On the microscope stage, a circular pad marked with a measurement scale (marked in millimeters) radiated out from a central point. The tube was placed flush in the center of the measurement scale, and the sand was installed. The tube was raised slowly and steadily until all sand exited. The distance from the center of the scale to the edge of the resultant sand cone was recorded at eight locations and the height of the sand cone measured using calipers to the nearest millimeter. This process was repeated three times, and the average radius and cone height were used to calculate angle of repose. Additionally, each sand was evaluated visually for overall particle shape and color using angularity/ sphericity and Munsell color charts, respectively (data not presented).

The particle size distribution of each sand was used to calculate geometric mean diameter, coefficient of uniformity and gradation index. In addition to the bunker sand materials, three materials were included for general comparison; these

TABLE 1. Particle size distribution and calculated physical properties of commercially available sand materials from various regions in the United States.

		Partic	e size dis	tribution Calculated property							
Sand	>2.0	1.0	0.5	0.25	0.15	0.1	0.05	<0.05	GMD†	Cu‡	GI§
			g/kg ¹ unitless			ess					
Autumn Gold	7	45	64	532	305	24	9	15	0.60	2.00	3.24
Bunker	1	79	261	375	217	27	29	11	0.66	3.63	2.00
Caylor White	3	46	193	599	127	9	5	18	0.66	1.82	3.32
Crushed Limestone	3	363	548	67	11	3	4	1	0.95	1.86	3.53
Extra Firm Bunker	1	59	198	337	263	76	48	17	0.59	2.85	6.23
Fine Topdressing	0	2	2	127	462	190	165	53	0.35	3.60	2.40
Glass beads	0	0	296	704	0	0	0	0	0.71	1.61	2.57
Gray Walreth Double Wash	0	17	204	584	137	16	12	30	0.63	2.22	3.83
Green Plus	6	130	270	448	110	6	5	26	0.71	2.38	5.24
Holliday (Banner Springs)	2	24	173	545	191	38	23	4	0.63	3.94	2.24
Holliday (Miss. River)	1	55	270	533	137	3	0	0	0.70	3.70	1.91
Klassic White	8	77	173	515	206	6	3	12	0.67	2.11	4.74
Kosse White	2	6	37	372	518	37	13	14	0.54	1.47	2.41
Orlando White	4	31	108	430	314	41	20	52	0.55	2.20	3.87
Pro/Angle	10	163	328	281	149	30	19	21	0.72	3.33	7.78
Pro White Bunker	0	8	86	649	204	21	10	21	0.60	2.50	4.69
Putting Green	0	48	324	503	84	14	14	13	0.70	5.28	2.56
Shelby Bunker	9	69	306	473	121	6	4	12	0.71	2.00	3.79
Sidley 1600	10	12	70	415	379	77	35	2	0.56	2.25	4.17
Stone White	0	0	0	350	555	40	14	41	0.50	1.53	2.53
Tan Bunker	3	58	410	401	81	13	10	23	0.71	2.43	3.96
Tour Grade 50/50	43	184	190	307	192	24	· 13	47	0.68	2.72	8.89
Tour Grade 535	0	14	59	493	370	28	23	12	0.57	1.82	2.76
Tour Grade Signature	58	193	190	315	181	23	17	22	0.71	3.06	8.89
USGA Bunker	0	35	220	495	194	19	10	27	0.63	2.35	8.41
White Bunker	0	35	227	462	197	39	25	14	0.63	4.76	2.65

† Geometric mean particle diameter (GMD) = calculated from the sand particle size distribution.

‡ Cu (Coefficient of uniformity) = where D60/D10; "acceptable value" = 2 to 4, higher value = less uniformity, optimum value = 2 to 3, a value < 2 less likely to pack tightly.

§ GI (Gradation index) = where D90/D10; lower values indicate a higher potential for surface instability, acceptable range 3 to 6, preferred range 4 to 5.



••• ONE •••

INCREDIBLE FINISH

Respected names...trusted mowing performance...any way you choose to cut it... anywhere around the golf course...confidently expect the same great result...every time.

Visit us at the Golf Industry Show in Orlando, January 31–February 2, booth #3235.







www.nationalmower.com

m www.locketurf.com www.golfcourseindustry.com/readerservice - #54

www.gravely.com

"standards" included a medium-coarse putting green root-zone sand, a medium-fine topdressing sand and rounded laboratory glass beads.

WHAT WE DISCOVERED

During this laboratory study, we evaluated a variety of commercially available sand products from several regions of the United States. The sands included naturally mined sands, screened and washed sands, as well as some manufactured sands generated by a rock-crushing process. In addition to the bunker sand products, three sandsized materials were included for general comparison. These "standards" included a putting green root-zone sand, a fine sand topdressing and laboratory glass beads. All sands were evaluated

TABLE 2. Sand particle shape characteristics, calculated physical properties, and angle of repose of commercially available sand materials from various regions in the United States.

Sand	Sphericity	Angularity	GMD†	Cu‡	GI§	Angle of repose
			- mm-			- degrees -
Autumn Gold	Medium	Subangular	0.60	2.00	3.24	30.3
Bunker #1	Medium	Subangular	0.66	3.63	2.00	31.1
Bunker #2	Medium	Subrounded	0.63	2.35	8.41	30.9
Caylor White	Low	Angular	0.66	1.82	3.32	32.5
Crushed Limestone	Medium	Angular	0.95	1.86	3.53	34.9
Extra Firm Bunker	Medium	Subangular	0.59	2.85	6.23	31.6
Fine Topdressing	Medium	Subrounded	0.35	3.60	2.40	30.4
Glass beads	High	Rounded	0.71	1.61	2.57	21.8
Gray Double Wash	Medium	Subangular	0.63	2.22	3.83	34.4
Green Plus	Medium	Subangular	0.71	2.38	5.24	33.1
Holliday (Banner Springs)	Medium	Subangular	0.63	3.94	2.24	32.0
Holliday (Miss. River)	Medium	Subangular	0.70	3.70	1.91	31.4
Klassic White	Low	Angular	0.67	2.11	4.74	34.8
Kosse White	Medium	Rounded	0.54	1.47	2.41	30.8
Orlando White	Medium	Subangular	0.55	2.20	3.87	31.6
Pro/Angle	Medium	Very angular	0.72	3.33	7.78	33.1
Pro White Bunker	Low	Very angular	0.60	2.50	4.69	33.4
Putting Green	Medium	Subangular	0.70	5.28	2.56	32.2
Shelby Bunker	Medium	Subrounded	0.71	2.00	3.79	31.6
Sidley 1600	Medium	Subangular	0.56	2.25	4.17	32.4
Stone White	Medium	Subangular	0.50	1.53	2.53	32.9
Tan Bunker	Medium	Subangular	0.71	2.43	3.96	34.2
Tour Grade 50/50	Medium	Subangular	0.68	2.72	8.89	35.4
Tour Grade 535	Medium	Subangular	0.57	1.82	2.76	30.7
Tour Grade Signature	Low	Angular	0.71	3.06	8.89	33.9
White Bunker	Medium	Subangular	0.63	4.76	2.65	34.6

† Geometric mean particle diameter (GMD) = calculated from the sand particle size distribution.
 ‡ Cu (Coefficient of uniformity) = where D60/D10; "acceptable value" = 2 to 4, higher value = less uniformity, optimum value = 2 to 3, a value < 2 less likely to pack tightly.

GI (Gradation index) = where D90/D10; lower values indicate a higher potential for surface instability, acceptable range 3 to 6, preferred range 4 to 5.

for visual characteristics, such as particle shape and color, and also for their general physical properties (Table 1).

As expected, sand color varied widely, ranging from white to cream, tan and brown (data not presented). Of all selection characteristics, color appears to be the most subjective criteria and should be one of the last factors considered when selecting a sand for bunker use. Probably one of the more routine measurements conducted on sands is determining the sand's particle size distribution. Once the particle size distribution is determined, this data can sometimes be used to infer physical performance characteristics. Three properties - geometric mean diameter, the coefficient of uniformity and gradation index - were calculated from the particle size distribution. As expected, there was a wide range in particle size distribution which resulted in guite a bit of variation in the associated calculated values.

For geometric mean diameter, which is one method for distilling a particle size distribution down into a single value and provides an overall sense for the relative coarseness or fineness of the sand, values ranged from 0.35 millimeter to 0.95 millimeter (Table 1). Although this is a convenient method for reducing a particle size distribution down into a single manageable value, it also can be somewhat misleading. For example, the laboratory glass beads had a very narrow particle size distribution with 100 percent of the particles in the 0.5-millimeter and 0.25-millimeter size classes, and a geometric mean diameter of 0.71. This value was similar to five other sand materials including the standard putting green sand (GMD equals 0.70), which contained a much wider range of particle size classes.

Based on the very narrow particle size distribution of the glass beads, it's predicted this material would be rather unstable or soft, simply because of the lack of bigger or smaller size classes necessary to fill in voids around the existing two size classes and increase surface stability. In general, however, for a bunker sand, a minimum value greater than 0.5 millimeter is desirable. Below this value the sand might drain too slowly when installed in low lying bunker bottoms, resulting in wet or soft playing conditions.

For the coefficient of uniformity, which is a numerical expression of how uniform the particle sizes are and another value that could be used to predict how likely sand particles are to pack, the values ranged from 1.47 to 5.28. Some

syngenta

Just because it's a rough area doesn't mean two turfgrasses should be allowed to fight.

A course at peace looks good and plays well. Harness the power of Tenacity[™] herbicide for systemic, selective pre- and post-emergence control of 46 broadleaf weed and grass species, including creeping bentgrass in Kentucky bluegrass, perennial ryegrass, and fescue. Keep the peace by keeping grasses separated.

Visit www.TenacityHerbicide.com for more information on all the ways Tenacity can benefit your course, and for a list of weeds and grasses controlled, plus an interactive training guide.



www.SyngentaProfessionalProducts.com

©2008 Syngenta Syngenta Professional Products, Greensboro, NC 27419. Important: Always read and follow label instructions before buying or using this product. Tenacity" is not currently registered for use in all states. Please check with your state or local extension service prior to buying or using this product. Tenacity" and the Syngenta logo are

references suggest that "acceptable" coefficient of uniformity values are between 2 and 4. In general, a higher value suggests less uniformity and a greater range of particle sizes. Coefficient of uniformity values below 2 suggest a tendency for the particles to pack less tightly. Of the sands evaluated, 19 of the 26 sands fell within the "acceptable" range.

A similar calculated property is the gradation index, for which values ranged from 1.91 to 8.89. For gradation index values, lower values indicate a higher potential for surface instability with a suggested "acceptable range" of 3 to 6, and a preferred range of 4 to 5. For these sands, 11 of the 26 fell in the "acceptable" range, and only three were in the "preferred" range: Green Plus, Pro White and Sidley 1600.

In addition to analysis of data associated with the particle size distribution, visual inspection of the sand particles resulted in a substantial variation. For sphericity or roundness, the sands ranged from low to high, with most sands possessing a medium sphericity. The laboratory glass beads were highly spherical. For angularity, the sands ranged from subangular to very angular, with the majority of sands possessing a subangular shape. In general, a more angular and less rounded sand tends to pack tightly and result in a desirable firm sand characteristic.

One additional measurement that might help laboratories predict sand firmness is the angle of repose (Table 2). This calculation, expressed in



www.golfcourseindustry.com/readerservice - #56



The data most helpful for determining surface hardness is the modified pocket penetrometer test.

degrees, is derived from measuring the mean diameter of the base and apex height of a dry sand cone. As one would expect, coarser textured, more angular sands with wider particle size distributions are more likely to stack higher, resulting in a narrower base and taller cone apex and ultimately a greater angle of repose. For the sands evaluated in this study, the angle of repose values ranged from 21.8 degrees to 35.4 degrees. The lowest values occurred for the rounded laboratory glass beads and the highest value was associated with Tour Grade 50/50. Most sands had an angle of repose between 31 and 32 degrees.

PHYSICAL PROPERTIES AND SAND FIRMNESS

Besides the highly subjective characteristic, color, an important bunker sand property is firmness manifested as resistance to golf ball penetration. The values for the modified pocket penetrometer ranged from 1.22 to 3.31 kilograms per square centimeter, with values of 1.66 kilograms per square centimeter and 1.59 kilograms per square centimeter for the mean and median penetrometer values, respectively (data not presented).

In data interpretation, the scale most often used is presented in Table 3. This scale indicates that a lower threshold of 1.8 kilograms per square centimeter and below is the value most prone to producing a buried or plugged golf ball lie. Of the sands evaluated, 10 sands had a penetrometer value greater than 1.8 kilograms per square centimeter, but the majority of the sands were between 1.2 kilograms per square centimeter and 2.2 kilograms per square centimeter. As expected, the rounded laboratory glass beads with a narrow particle size distribution and spherical shape had the lowest penetrometer value of 0.1 kilograms per square centimeter than 2.2 kilograms per square centimeter and 2.2 kilograms per square centimeter. As expected, the rounded laboratory glass beads with a narrow particle size distribution and spherical shape had the lowest penetrometer value of 0.1 kilograms per square centimeter ter and would be considered "softest." Generally, values greater than 2.2 kilograms per square centimeter are desirable because above this value the sand will most likely only have a slight or no tendency to produce a buried golf ball lie (Table 3).

CONCLUSION

When evaluating all the physical data for these bunker sands, no single measured or calculated property (e.g., the coefficient of uniformity

Know the Sign.



Greater Than Or Equal To.

Quali-Pro products feature formulation quality second to none for performance results equal to the competitive brands they replace.

NEW Fosetyl-Al 80 WDG. With the same active ingredient as Aliette WDG, new Fosetyl-Al delivers excellent systemic control of Pythium, *Rhizoctonia*, and other diseases. Learn more at **quali-pro.com**.



Professional Turf & Ornamental Products

©2008 FarmSaver.com, LLC. Quali-Pro is a registered trademark of FarmSaver.com. Aliette is a registered trademark of Bayer. Always read and follow label directions.

or angle of repose) was a strong indicator or predictor for penetrometer values. Although 10 sands had penetrometer values greater than 1.8 kilograms per square centimeter, which is the suggested threshold for an "acceptable" dry sand firmness value, only five sands were greater than 2.2 kilograms per square centimeter. In an attempt to relate these physical property data to penetrometer values, linear regression was conducted with the gradation index, coefficient of uniformity and angle of repose data. The results of these analyses resulted in R2 values of 0.0715, 0.0051 and 0.2566, for the gradation index, coefficient of uniformity and angle of repose data, respectively. In other words, because of the high degree of variability, there was little to no relationship between these properties and sand surface firmness.

As an example of the variability present in these sand properties, one of the crushed sand products had the highest penetrometer value, 3.31, but also possessed a coefficient of uniformity and gradtion index value of 1.86 and 3.53, respectively. If one were to characterize this sand based solely on the coefficient of uniformity or gradation index data, they would predict this sand is less likely to pack because the coefficient of uniformity is less than 2.0 and that its surface instability is barely "acceptable" because of the gradation index value falling barely inside the 3 to 6 "suggested" range. Based on this information, it's apparent many properties likely influence sand surface hardness. These properties include particle size distribution, particle shape and other less quantifiable characteristics such

TABLE 3. Interpretation of modified penetrometer test values and their influence on performance characteristics for bunker sands (Thomas Turf Services), as well as the number of sands falling into the various firmness categories.

Penetrometer value (kg/cm²)	Potential for golf ball burying	Number of sands in each category
> 2.4	Very low tendency to bury	2
2.2 - 2.4	Slight tendency to bury	2
1.8 - 2.2	Moderate tendency to bury	6
< 1.8	High tendency to bury	15

as particle surface roughness.

Mechanically crushing minerals into sandsized products certainly affects surface roughness. This rough particle surface architecture might allow particles to bridge or link with adjacent particles better than smoother naturally occurring materials. By contrast, however, the use of rough or highly angular particles also might have negative effects on turf health, as there might be a higher chance for mechanical damage from turf abrasion when these sands are splashed onto putting greens and collars in locations where mowers turn sharply and often.

In summary, it's highly recommended to enlist the assistance of an accredited testing laboratory when evaluating sands for golf course bunker use. These laboratories can run a variety of physical analysis tests and be extremely helpful during the selection process. Besides the tests conducted in this study, these laboratories also can assess other properties like crusting potential, water retention and infiltration rate. Additionally, these



The sands analyzed in the study were variable in terms of all properties measured: particle size distribution, angularity, angle of repose, color and particle shape.

laboratories probably are familiar with many of the existing regionally available sands, which might have been characterized already.

To date, the procedure most used for evaluating surface hardness is the modified pocket penetrometer test. But this test has met with some criticism because of considerable variability in measurements among users. One important point to make regarding this measurement is that it's conducted using dry sand in a nonflexible box, conditions not normally exhibited in the field. In reality, sand is installed on slopes of various slope angles, with or without subsurface drainage, and at depths often exceeding three inches. All of these factors affect sand moisture content and ultimately, performance.

Additionally, sand in a typical bunker would rarely be subject to the lateral confinement that exists in the test box. Thus, if an individual were to take an in situ penetrometer measurement in a real bunker, the observed value would likely be softer than what was obtained under laboratory conditions. In response to this concern, alternative, more quantitative methods currently are under evaluation at several research laboratories. These methods include using various impact hammers, such as the Clegg impact tester, to test for sand firmness. It's the authors' hope a more reliable test will be developed and correlated with other sand physical properties. **GCI**

Cale Bigelow, Ph.D., is an assistant professor of agronomy at Purdue University in West Lafayette, Ind., and Douglas Smith, Ph.D., is an associate professor at USDA-ARS, National Soil Erosion Research Laboratory in West Lafayette, Ind.

Courtesy of USGA Turfgrass and Environmental Research Online (ISSN 1541-0277). Literature cited can be found on www.golfcourseindustry.com.

30 GREEN!



Seabore Paspalum

- Save drinking water: may be irrigated with effluent, even seawater
- Use less water
- Use salt to kill weeds
- Use less fertilizer
- Plays great, putts true with virtually NO GRAIN
- One grass tee-to-green

Grass your course with SeaDwarf, the Environmental Turfgrass

Visit **www.environmentalturf.com** or call 863-452-6595 to find a licensed sod producer near you



CONSTRUCTION EQUIPMENT

BY MARGARET HEPP

Equipped for perfection

Connecticut club perpetually improves its golf course

ost superintendents are able to breathe a sigh of relief after a big renovation. But Tony Girardi, CGCS, at the 18-hole Rockrimmon Country Club in Stamford, Conn., has been overseeing construction projects since he arrived there 14 years ago.

"We've been in every phase of golf course construction, whether it's building greens, tees or carpaths, reshaping fairways or expanding ponds," he says. "We've installed an irrigation system and pumping station. We've done it all."

Built in 1949 on an old family farm plot, members of the private facility hired Robert Trent Jones to design the first nine holes for \$7,500. The second nine holes were added in 1954, and a considerable renovation and addition took place in 1996.

With so much construction activity, Girardi no doubt would own a small fleet of equipment if he executed every project in-house. To maximize his \$1.3-million maintenance budget, he outsources large construction projects.

"Certain jobs – such as major greens construction, pond and creek restoration work, and reestablishing wetlands – are just overwhelming in regard to the construction equipment and manpower we would need," he says. "We've brought in just about every piece of equipment out there."

Hiring construction companies allows Girardi and his 19-man, in-season staff to focus on daily course maintenance, which still involves plenty of construction. Three years ago, Girardi decided to alleviate the stress on his John Deere front-end backhoe – 19 years old at the time – with a Bobcat 435 compact excavator. During the purchase process, he came across the Bobcat A300 skid steer and considered replacing both of his construction machines simultaneously.



The golf course at Rockrimmon has been through every phase of construction during the past 14 years, from rebuilding greens to USGA specs to improving internal drainage on existing native soil pushup greens (below). Photos: Rockrimmon Country Club

